

Device for the test irradiation of objects coated with photosensitive resists

5 The invention relates to a device for the test irradiation of objects coated with photosensitive resists having an EUV radiation source, an optical system for filtering the radiation from the EUV radiation source, a chamber for receiving the object and also means for interrupting the
10 beam path onto the object. The invention additionally relates to a method for operating such a device.

The term lithography denotes, in semiconductor technology, a method for transferring circuit patterns of microelectronic
15 components and integrated circuits onto a silicon semiconductor slice, the wafer. For this purpose, firstly a mask is produced which contains the pattern in the form of differences in transparency for the beams which are used to transfer said pattern onto the wafer. The wafer surface is
20 coated with a radiation-sensitive photoresist and exposed through the mask. Semiconductor structures are transferred onto the photoresist by means of a so-called lithography scanner. During the subsequent development, depending on whether a positive or negative resist is involved, the
25 exposed or unexposed photoresist is dissolved away and the wafer surface is uncovered at these locations.

On account of the decreasing feature size of semiconductors, the fabrication of modern semiconductor elements, such as,
30 for example, memory chips and CPUs, requires a resolution which makes it necessary to use extremely short-wave radiation of approximately 13 nm with a quantum energy of approximately 92 eV (EUV radiation). The irradiation wavelengths of 248 nm (UV radiation), 193 nm (DUV radiation)
35 or 157 nm (VUV radiation) used heretofore no longer suffice to produce the shrinking structures. As the feature size and wavelength decrease, however, there is an increase in the requirements made of the

resists used, the so-called resist material, as far as both the sensitivity and the line roughness are concerned.

5 The changed requirements made of resists require the test systems thereof to be adapted, said test systems being used to determine the resist properties with varying irradiation before series production of the wafers.

10 EUV radiation is absorbed by matter to an extremely high degree. It is necessary, therefore, for the EUV radiation to be guided under ultra-high vacuum conditions. The source of the EUV radiation is a thermally emitting plasma. In contrast to the lasers used heretofore, plasma emits in a very broad band, so that DUV, VUV and UV radiation are also
15 obtained besides the desired EUV radiation. It is necessary, therefore, to keep this radiation away from the resists by means of spectral filters.

20 So-called EUV beam tubes on synchrotron storage rings which emit monochromatized EUV radiation constitute a highly stable EUV radiation source for researching EUV lithography technology. Such EUV radiation sources emit very short radiation pulses (< 1 ns) with repetition frequencies of a few MHz, so that these EUV sources are often referred to as
25 quasi-cw sources. On EUV beam tubes on synchrotron storage rings, for the purpose of testing resists applied on slabs, individual fields have been irradiated sequentially with different radiation doses in order to determine the influence of the radiation dose on the resist. Moreover, on
30 synchrotron storage rings, a plurality of resist-coated fields have also already been exposed simultaneously, a rapidly rotating diaphragm wheel arranged upstream of the resist layer in the beam path performing the function of a neutral wedge filter. The diaphragm apertures arranged
35 radially on the wheel have different sizes, so that the individual fields are exposed to the radiation for different lengths of time during each revolution. Reproducible

radiation conditions on the individual fields of the object are only possible with the diaphragm wheel because the EUV radiation source exhibits virtually steady-state behavior on account of the high repetition frequency and radiates very
5 stably.

Finally, irradiation experiments on resists have already been carried out using low-power laboratory radiation sources for EUV radiation, in each case only an individual
10 field on the object having been irradiated. EUV laboratory radiation sources generate a dense and hot (> 200 000°C) plasma and emit the EUV radiation exclusively in very short pulses (typically 100 ns) with very low repetition rates (typically 10 - 1000 Hz).

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Taking this prior art as a departure point, the invention is based on the object of providing a device for the test irradiation of objects coated with photosensitive resists which, using an inexpensive radiation source, enables an at
20 least partly simultaneous irradiation of a plurality of irradiation fields on the object with varying dose in the shortest possible time and manages without complex and therefore costly optical systems in the beam path of the EUV radiation and in the case of which a degradation of the
25 optical elements in the beam path through EUV irradiation has no influence on the test result obtained.

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In the case of a device of the type mentioned in the introduction, this object is achieved by virtue of the fact
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- the EUV radiation source is a laboratory source for EUV radiation,
- the optical system has at least one filter for
35 suppressing undesirable spectral components of the radiation, in particular of VIS, UV, DUV, VUV radiation, and also at least one mirror for spectrally filtering the "in-band" EUV range,

- the means for interrupting the beam path comprise a plurality of closable diaphragm apertures which enable a temporal control of the irradiation of irradiation fields that lie on the object and are situated downstream of the diaphragm apertures, and
- 5 - the at least one monitor detector is arranged downstream of the optical system in the direction of the beam path and detects the radiation dose during irradiation.

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The laboratory source for EUV radiation is, by way of example, a low-power plasma-based source, e.g. an EUV lamp having a power of 100 W and a pulse frequency of 50 Hz according to the HCT (hollow cathode triggered) principle.

15 The laboratory source reliably makes the required EUV radiation available over a long operating period.

The plasma of the laboratory source emits highly broadband radiation that also contains DUV, VUV, UV and VIS radiation besides the desired EUV radiation. In order to suppress these undesired spectral components of the radiation, the optical system preferably has a spectral filter. The filter may comprise for example a thin metal film (e.g. a 150 nm thick zirconium film on a supporting grating). The filter is preferably situated at the exit opening of the laboratory source. By means of this arrangement, the filter prevents contaminants from the laboratory source from passing into the receiving chamber for the object to be irradiated and from soiling parts situated there.

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The optical system has the further task of ensuring that the irradiation is effected only with the "in-band" EUV radiation with a wavelength of 13.5 nm. A multilayer mirror, in particular, is suitable for filtering.

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The component parts of the optical system have the effect that practically only the desired EUV radiation impinges on the object.

The compact optical system of the device according to the invention, in particular with only a filter and a mirror, enables a very small distance between the EUV laboratory source and the object to be irradiated with homogeneous irradiation of all the irradiation fields. The small distance means that it is possible to utilize a large solid angle of the thermal emission of the plasma even without a complex condenser.

10 The diaphragm apertures that are closable according to the invention permit an at least partly simultaneous irradiation of the irradiation fields defined on the object through the diaphragm apertures. All the irradiation fields are initially irradiated in parallel until individual diaphragm apertures are closed after reaching the target dose for the assigned irradiation field. A considerable gain in time is thereby achieved when testing the influence of the irradiation dose on a photoresist.

20 The diaphragm apertures are preferably arranged in a planar plate and have a diameter of 5 mm, by way of example. With 20 diaphragm apertures of this type, the test duration for a photoresist can be reduced almost by a factor of 20 compared with individual irradiations with different radiation doses.

25 After a calibration that is carried out beforehand, the monitor detectors arranged downstream of the optical system permit an exact measurement of the irradiation dose of the individual irradiation fields. By way of example, a plurality of photodiodes (Schottky type) may be used as monitor detectors. The signals supplied by the diodes are preferably averaged in order to improve the measurement accuracy. By continuously detecting the irradiation dose during irradiation, the irradiation of the irradiation fields can be carried out with precisely definable desired values for the irradiation dose.

The monitor detectors are preferably arranged between the optical system and the closable apertures; they are expediently situated as near as possible to the object to be irradiated. This arrangement of the monitor detectors makes
5 the device insensitive to the degradation of the optical system.

As already mentioned in the introduction, the entire beam path has to be guided up to the object under vacuum
10 conditions. Therefore, the chamber for receiving the object is designed for and evacuated to a negative pressure of 10^{-6} m bar for example. It is separated from the discharge chamber of the laboratory source by a window having an opening for the passage of the radiation, a filter of the
15 optical system, for example in the form of a metallic film, being situated, in particular, in the window. This prevents contamination of the receiving chamber. The receiving chamber preferably has a dedicated pump system and, when the object to be irradiated is being handled, is separated by
20 means of a slide valve from the laboratory source and preferably also the region for receiving the optical system.

In order to obtain an irradiation that is as homogeneous as possible in the individual irradiation fields, all the
25 diaphragm apertures are arranged in one plane and the irradiation fields produced on the object through each diaphragm aperture do not overlap. The irradiation fields are preferably arranged parallel to the plane of the diaphragm apertures.

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The object coated with photoresist is, in particular, a silicon wafer, for example a 6 inch wafer having a thickness of 650 μm and having 20 irradiation fields defined by the diaphragm apertures. A mount is situated in the receiving
35 chamber and receives the wafer in such a way

that the EUV radiation impinges on the photoresist coating thereof.

5 In an expedient refinement of the invention, the laboratory source emits radiation pulses having a duration of less than 1 μ s, in particular 100 ns, with a repetition rate of between 1 and 10000 Hz, in particular 1 - 5000 Hz. The radiation of the laboratory source originates from a thermally emitting plasma, in particular from a laser-
10 generated or discharge-generated plasma or from an electron beam.

Preferably, a thin metal film, in particular a zirconium film having a thickness of less than 200 nm but more than
15 100 nm, is arranged in the beam path as filter for suppressing undesirable visible to VUV radiation. The film transmits up to 50% of the desired EUV radiation, while the undesirable radiation is suppressed by a factor of > 1000.

20 Each mirror for spectrally filtering the "in-band" EUV range is preferably configured as a multilayer mirror, in which case the mirror may be embodied as a plane mirror or as a curved mirror. The multilayer mirrors reflect up to 70% of the incident radiation in a narrow spectral band in the EUV
25 range, while radiation that does not lie in this narrow band is almost completely absorbed by the multilayer mirror.

The diaphragm apertures are preferably closed by means of a flat slide which is arranged such that it can be displaced
30 in a plane parallel to the plane of the diaphragm apertures and has a contour enabling successive opening or closing of the diaphragm apertures. The contour is staircase-shaped, in particular, thereby enabling a row-by-row opening or closing of the diaphragm apertures arranged in rows. The flat slide
35 as closure for all the diaphragm apertures, with only one

mechanical component, constitutes a solution that is highly expedient in terms of construction and control technology.

Further advantages and effects of the invention and also the operating procedure thereof emerge from the following description of an exemplary embodiment with reference to the figures.

In the figures:

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figure 1 shows the spectrum of the radiation generated by the EUV radiation source

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figure 2 shows a basic illustration of the device according to the invention for the test irradiation of objects coated with photosensitive resists

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figure 3 shows a diaphragm system with a flat slide arranged in the device according to figure 2

figure 4 shows an irradiation function with a variation of 50% with different exponents, and

figure 5 shows an illustration of the film thickness of a resist application as a function of the dose of a test irradiation.

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The device for EUV test irradiation serves for examining a photoresist (resist) for lithography in the range of EUV radiation, i.e. at a wavelength of 13.5 nm, with 20 different radiation doses in one work operation. In this case, the intention is to determine the removal of the photoresist after development and the sharpness of the imaged structures depending on the dose.

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The device for EUV test irradiation comprises an EUV laboratory lamp (1), which generates a radiation having a spectrum according to figure 1. Via a horizontally oriented beam tube (2) with an exit opening (3), the likewise horizontally oriented beam path (4) leaves the EUV laboratory lamp (1).

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A beam tube slide unit (5) is arranged at the exit opening (3). The beam tube slide has a passage into which a 150 nm thick zirconium film is inserted, which can be moved into the beam path (4) by means of the slide. The slide, which is
5 movable transversely with respect to the axis of the beam path (4), permits the zirconium film to be completely moved out of the cross section of the beam tube (2), so that the exit opening (3) is completely closed by the beam tube slide, which incidentally is composed of metal. Furthermore,
10 a turbomolecular pump (6) is arranged at the beam tube (2) and generates a vacuum of approximately 10^{-3} mbar in the EUV lamp (1) with a xenon atmosphere being maintained.

The beam tube slide unit (5) is adjoined by a hollow-cylindrical elbow (7), which receives a deflection mirror (8). The deflection mirror (8) is arranged in the interior
15 of the elbow in the outer region of the angled-away portion in such a way that the horizontally impinging beam path (4) is deflected by 90° into a wafer chamber (9), which is designated in its entirety by (9). A mirror receptacle (11)
20 carries and fixes the deflection mirror (8). It is pointed out that the constructionally expedient angle of incidence of the EUV radiation of 45° illustrated in the exemplary embodiment can readily be varied.

25 The elbow (7) is adjoined by the wafer chamber (9), which comprises a hollow-cylindrical beam tube (12) and also a receiving space (13) for the resist-coated wafer. The beam path (4) propagates proceeding from the deflection mirror (8) through the beam tube (12) in the direction of a
30 diaphragm system (15). The wafer is oriented with its resist surface in the direction of the diaphragm system (15), so that the EUV radiation that passes through the diaphragm system falls onto the resist coating of the wafer. The
35 closure of the diaphragm apertures of the diaphragm system (15) is driven by a stepper motor (14).

A further turbomolecular pump (17) is arranged laterally at the receiving space (13) and, during the exposure, ensures that a pressure of 10^{-6} mbar is maintained in the elbow (7) and also the wafer chamber (9).

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Three photodiodes (18) are situated in the direction of propagation of the beam path (4) of the EUV radiation laterally in the diaphragm system (15), which photodiodes can be discerned in figure 3 and detect the radiation energy of the individual radiation pulses of the EUV lamp (1), the radiation energy being proportional to the charge generated in the photodiodes (18). The photodiodes are arranged at the least possible distance from the diaphragm apertures in the diaphragm system, but in such a way that they are not
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15 concealed by the motor-driven closure.

Finally, the device for EUV test irradiation has a further slide (19) arranged between the elbow (7) and the beam tube (12) of the wafer chamber (9). If the slide (19) is closed, the wafer chamber (9) is completely partitioned from the EUV lamp (1) and the interior space of the elbow (7).
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Figure 3 illustrates the construction of the diaphragm system, which is designated in its entirety by (15) and has a perforated mask (21) with 5 rows each having 4 diaphragm apertures (22). The EUV radiation passing through each diaphragm aperture (22) defines a demarcated irradiation field on the resist layer (16) of the wafer. The distance between wafer and diaphragm system (15) and also the distance between the diaphragm apertures (22) are designed such that the irradiation fields do not overlap. As a result, the diaphragm system (15) produces twenty demarcated irradiation fields having a diameter of approximately 5 mm on the surface of the wafer coated with photoresist.
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A flat slide (24) having a staircase-shaped contour (23) at the end is situated laterally beside the perforated mask

(21). On the opposite side from the contour (23), the flat slide (24) is connected to the stepper motor (14) illustrated in figure 2. By moving the flat slide (24) in the direction of the arrow (25), it is possible for the diaphragm apertures (22) to be mechanically closed one after the other row by row. The consequence of this is that the irradiation fields defined by the individual diaphragm apertures (22) acquire individual irradiation times.

10 During the irradiation of the coated wafer, the slide of the beam tube slide unit (5) is pushed in such that the beam path passes through the zirconium filter. In this case, the filter has two functions:

- 15 1. Holding back radiations having wavelengths of greater than 20 nm. At wavelengths of greater than 20 nm, the transmissivity of the zirconium filter is less than 10%.
- 20 2. Separating the xenon atmosphere in the EUV lamp (1) from the region which is formed by the elbow (7) and the wafer chamber (9) and into which no xenon gas should pass. The zirconium filter is stable enough to withstand the pressure difference between the EUV lamp (1) and the aforementioned region.

25 The deflection mirror (8) is a multilayer mirror having, for example, 40 layers of a silicon substrate with a period thickness of approximately 10 nm. This mirror reflects a wavelength of 13.5 +/- 0.2 nm at an angle of 45° into the beam tube (12) of the wafer chamber (9).

30 After the conclusion of the irradiation of the photoresist on the wafer, the slide (19) between the elbow (7) and the wafer chamber is closed. As a result, the vacuum is preserved in the EUV lamp (1) and the elbow (7) if the wafer chamber (9) is ventilated in order to open the latter for example for the purpose of removing the irradiated wafer. The slide (19) enables not only shorter evacuation times of the wafer chamber

(9) during wafer handling, but furthermore an effective protection of the sensitive optical system that is formed by the zirconium film in the beam tube slide unit (5) and the deflection mirror (8) in the elbow.

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The photodiodes (18) arranged in the beam path (4) in the perforated mask (21) measure the radiation energy of the EUV radiation pulses in that they generate a charge proportional to the radiation energy in the photodiodes. The charge
10 generated by the individual pulses is added up electronically and cyclically interrogated by a controller (not illustrated in the figure). If the interrogation reveals that a specific radiation dose (desired value) has been reached, a control command is initiated for the stepper
15 motor (14), which moves the flat slide (24) in the direction of the arrow (25) in order to close the next diaphragm aperture (22) row by row. The desired values that have to be reached depending on a target dose prescribed by the user (definition: a dose which the user of the test system
20 assumes to be optimal for the resist to be examined) before the next diaphragm aperture (22) is closed form the discrete points of an irradiation function. The individual desired values are calculated according to the following formula:

if $s \neq 10$ then:

$$s(F, \text{Exp}, \text{Tar}, \text{Var}) = \text{Tar} \left(1 + \text{VB} \frac{|\text{RF}|}{\text{RF} - 10} \left(\frac{|\text{RF}|}{\text{RF} - 10} \right)^{\text{Exp}} \right)$$

$$\text{where } \text{VB} = \frac{\text{Var}}{100} \text{ and } \text{RF} = F - 10$$

otherwise:

$$s(F, \text{Exp}, \text{Tar}, \text{Var}) = \text{Tar}$$

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The following are applicable in this case:

- s** The function value s is the desired value that has to be reached before the next diaphragm aperture is
30 closed.
- F** The parameter F represents the currently closed field and lies in the range of values from 1 to 20.

Exp The parameter Exp is the exponent set by the user and has the values of 1 to 5.

Tar The parameter Tar is the target dose set by the user.

Var The parameter Var is the variation range set by the user in percent in the range from 1 to 100.

For Tar:=1.0 and Var:=50, the characteristic curves shown in fig. 4 result depending on the exponent Exp:=1 to 5 for the desired values s. It becomes clear that the density of discrete points around the target dose Tar increases as the exponent Exp increases.

The irradiation with EUV radiation brings about a removal of the resist film after the development on the wafer. The relationship between dose and removal after the development is illustrated in the curve according to fig. 5 using the example of a concrete resist. The value for the residual thickness of the resist film falls sharply starting from a specific dose. The minimum dose required for the irradiation of this resist (approximately 6 mJ/cm² in the exemplary embodiment) can be read from the x axis. In this way, it is possible to determine the EUV radiation sensitivity of a photoresist for wafers in one work operation.

List of reference symbols:

EUV lamp	1
Beam tube	2
Exit opening	3
Beam path	4
Beam tube slide unit	5
Turbomolecular pump	6
Elbow	7
Deflection mirror	8
Wafer chamber	9
--	10
Mirror receptacle	11
Beam tube	12
Receiving space	13
Stepper motor	14
Diaphragm system	15
Wafer with resist layer	16
Turbomolecular pump	17
Photodiodes	18
Slide	19
--	20
Perforated mask	21
Diaphragm apertures	22
Staircase-shaped contour	23
Flat slide	24
Arrow	25